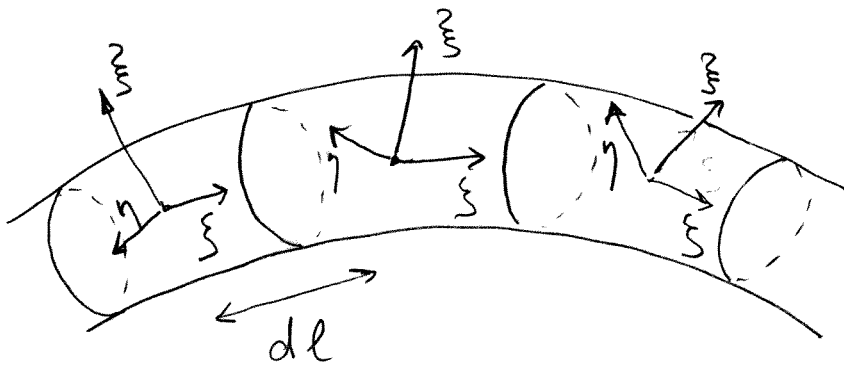


The energy of a deformed rod

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General description

We divide the rod into infinitesimal elements bounded by two adjacent cross-sections. For each of these elements we use a coordinate system $\{\xi, \eta, \zeta\}$. ζ axis is parallel to the axis of the rod. All the systems are parallel in the undeformed state.



Let $d\vec{\varphi}$ be the vector of the angle of relative rotations of the two systems at a distance dl apart. Deformation is determined by the rate of rotation of the coordinate axes along the rod $\frac{d\vec{\varphi}}{dl}$.

We can construct quadratic form out of $\frac{d\vec{\varphi}}{d\ell}$ (41)

$$F = \int \left[\frac{1}{2} I_1 E \left(\frac{d\varphi_z}{d\ell} \right)^2 + \frac{1}{2} I_2 E \left(\frac{d\varphi_\eta}{d\ell} \right)^2 + \frac{1}{2} C \left(\frac{d\varphi_\xi}{d\ell} \right)^2 \right] d\ell$$

First two terms in the expression above can be written as $\int \left[\frac{1}{2} I_1 E \left(\frac{d\vec{\tau}_\eta}{d\ell} \right)^2 + \frac{I_2 E}{2} \left(\frac{d\tau_z}{d\ell} \right)^2 \right] d\ell$

Here $\vec{\tau}$ is tangential to the rod, regarded as elastic line. These two terms correspond to the bending of the rod. For the slight bending

we can approximate $\vec{\tau} = \frac{d\vec{r}}{d\ell} \approx \frac{d\vec{r}}{dx}$

and $\frac{d\vec{\tau}}{d\ell} \approx \left(\frac{d^2 z}{dx^2}, \frac{d^2 y}{dx^2} \right)$.

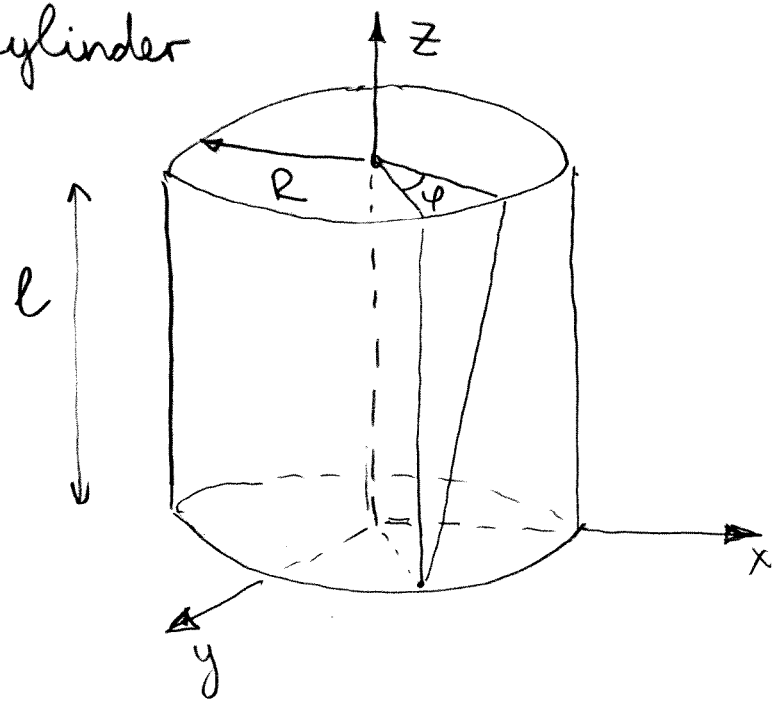
Then we arrive to the energy expression given at the p. 35.

The term $\frac{C}{2} \left(\frac{d\varphi}{dz} \right)^2$ corresponds to another kind of deformation - twisting or torsion.

In this case each cross-section is rotated about the axis of the rod.

Let us consider such deformation for a

Cylinder



Under rotation on angle φ $\vec{\delta r} = \vec{\delta \varphi} \times \vec{r} \Rightarrow$
 $\Rightarrow u_x = -y \varphi(z), u_y = x \varphi(z)$

In general u_z may not be zero, but for the cylinder one can see that $u_z = 0$

Note, that for torsion

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$\text{div } \vec{u} = 0 \Rightarrow$ pure shear deformation

Then equilibrium equation is

$$\mu \frac{\partial^2 u_i}{\partial x_k \partial x_k} = \mu \nabla^2 \vec{u} = 0$$

substituting $u_x = -y \varphi(z)$, $u_y = x \varphi(z)$

we obtain

$$\frac{d^2 \varphi(z)}{dz^2} = 0 \Rightarrow \varphi(z) = \varphi_0 \frac{z}{l}$$

$$u_{xz} = -\frac{y}{2} \frac{d\varphi}{dz}, \quad u_{yz} = \frac{x}{2} \frac{d\varphi}{dz}, \quad \text{other } u_{ik} = 0$$

$$\text{Then } \sigma_{xz} = 2\mu u_{xz} = -\mu y \frac{d\varphi}{dz}, \quad \sigma_{yz} = 2\mu u_{yz} = \mu x \frac{d\varphi}{dz}$$

$$F = \int dz \int d^2 r (\mu u_{ik}^2) = 2\mu \int (u_{xz}^2 + u_{yz}^2) d^2 r dz =$$

$$= \mu \int dz \int d^2 r \left(\frac{d\varphi}{dz}\right)^2 \frac{x^2 + y^2}{2} = \frac{\pi R^4}{2} \mu \int \frac{1}{2} \left(\frac{d\varphi}{dz}\right)^2 dz$$

$$= \frac{C}{2} \int \left(\frac{d\varphi}{dz}\right)^2 dz, \quad \text{where the torsional rigidity}$$

$$C = \frac{\pi}{2} \mu R^4$$

Assume that the bottom of the cylinder is fixed. What is the torque M that one needs to apply in order to twist the top on the angle φ_0 ?

$$\text{Energy is } \int \left[\frac{1}{2} C \left(\frac{d\varphi}{dz} \right)^2 dz + \mathcal{U} \right],$$

where \mathcal{U} is the energy due to external force.

varying with respect to φ we find

$$\int C \frac{d\varphi}{dz} \frac{d\delta\varphi}{dz} dz + \delta\mathcal{U} = 0$$

integrating by parts

$$-C \int \frac{d^2\varphi}{dz^2} \delta\varphi dz + C \frac{d\varphi}{dz} \delta\varphi \Big|_0^l + \delta\mathcal{U}$$

Since $\delta\mathcal{U} = -M \delta\varphi$ we obtain

$$-C \int \frac{d^2\varphi}{dz^2} \delta\varphi dz + \varphi_0 \left[C \frac{d\varphi}{dz} - M \right] = 0$$

In the first term $\delta\varphi$ is arbitrary $\Rightarrow \frac{d^2\varphi}{dz^2} = 0$

From the last term we get

$$M = C \frac{d\varphi}{dz} = \frac{\pi}{2} \frac{M \varphi_0 R^4}{l}$$